## **Ultra-Compact, 1.5A Thermoelectric Cooler (TEC) Controller**

### <span id="page-0-0"></span>**GENERAL DESCRIPTION**

The SLM8834 is a monolithic TEC controller with an integrated TEC controller. It has a linear power stage, a pulse-width modulation (PWM) power stage, and two zero-drift, rail-to-rail operational amplifiers.

The linear controller works with the PWM driver to control the internal power MOSFETs in an H-bridge configuration. By measuring the thermal sensor feedback voltage and using the integrated operational amplifiers as a proportional integral differential (PID) compensator to condition the signal, the SLM8834 drives current through a TEC to settle the temperature of a laser diode or a passive component attached to the TEC module to the programmed target temperature.

The SLM8834 supports negative temperature coefficient (NTC) thermistors as well as positive temperature coefficient (PTC) resistive temperature detectors (RTD). The target temperature is set as an analog voltage input either from a digital-to-analog converter (DAC) or from an external resistor divider.

The temperature control loop of the SLM8834 is stabilized by PID compensation utilizing the built in, zero drift chopper amplifiers. The internal 2.50 V reference voltage provides a 1% accurate output that is used to bias a thermistor temperature sensing bridge as well as a voltage divider network to program the maximum TEC current and voltage limits for both the heating and cooling modes. With the zero drift chopper amplifiers, extremely good long-term temperature stability is maintained via an autonomous analog temperature control loop.

### <span id="page-0-1"></span>**FEATURES**

- Integrated super low R<sub>DSON</sub> MOSFETs for the TEC controller
- High efficiency single inductor architecture
- TEC voltage and current operation monitoring
- No external sense resistor required
- Independent TEC heating and cooling current limit settings
- Programmable maximum TEC voltage
- 2.0 MHz PWM driver switching frequency
- **External synchronization**
- Two integrated, zero drift, rail-to-rail chopper amplifiers
- Capable of NTC or RTD thermal sensors
- 2.50 V reference output with 1% accuracy
- Temperature lock indicator
- Available in a 25-ball, 2.5 mm × 2.5 mm WLCSP or in a 24-lead, 4 mm  $\times$  4 mm QFN

#### <span id="page-0-2"></span>**APPLICATIONS**

- TEC temperature control
- Optical modules
- Optical fiber amplifiers
- Optical networking systems
- Instruments requiring TEC temperature control



#### <span id="page-0-3"></span>**SYSTEM BLOCK DIAGRAM**

## <span id="page-1-0"></span>**TYPICAL APPLICATION CIRCUIT**





<span id="page-1-2"></span><span id="page-1-1"></span>

## **Table of Contents**



## <span id="page-3-0"></span>**PIN CONFIGURATION**



## <span id="page-3-1"></span>**PIN DESCRIPTION**





N/A<sup>1</sup> : Not Available.

## <span id="page-4-0"></span>**ORDERING INFORMATION**



## <span id="page-5-0"></span>**ABSOLUTE MAXIMUM RATINGS**



#### **Note:**

Stresses beyond those listed under "Absolute Maximum Ratings" may cause permanent damage to the device. These are stress ratings only and functional operation of the device at these or any other condition beyond those indicated in the operational sections of the specifications is not implied. Exposure to absolute maximum rating conditions for extended periods may affect device reliability.

## <span id="page-5-1"></span>**RECOMMENDED OPERATION CONDITIONS**



## <span id="page-5-2"></span>**QUALIFICATION RATINGS**



## <span id="page-5-3"></span>**THERMAL INFORMATION**



## <span id="page-6-0"></span>**ELECTRICAL CHARACTERISTICS**

Test condition is V<sub>PVIN</sub> = V<sub>VDD</sub> =5V, V<sub>PVINL</sub> = V<sub>PVINS</sub> = V<sub>VDD</sub> =5V, T」= −40°C ~ +125°C for minimum/maximum specifications, and  $T_A = 25^{\circ}C$  for typical specifications, unless otherwise specified.



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## <span id="page-10-0"></span>**TYPICAL PERFORMANCE CHARACTERISTICS**

 $T_A = 25^{\circ}$ C, unless otherwise specified.







Figure 6. Efficiency vs. ITEC at VIN=3.3V and 5.0V with 2Ω Load in Cooling Mode





Figure 5. Efficiency vs. ITEC at VIN=3.3V in Heating Mode



Figure 7. Efficiency vs. ITEC at VIN=3.3V and 5.0V with 2Ω Load in Heating Mode





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Figure 10. Cooling to Heating Transient CH2: LDR (TEC+), CH3: SFB (TEC-), CH4: ITEC



Figure 12. Zero Acrossing TEC Current Zoom-in from Cooling to Heating CH2: LDR (TEC+), CH3: SFB (TEC-), CH4: ITEC



Figure 11. Zero Acrossing TEC Current Zoom-in from Heating to Cooling CH2: LDR (TEC+), CH3: SFB (TEC-), CH4: ITEC

## <span id="page-12-0"></span>**APPLICATION INFORMATION**

The SLM8834 is a single chip TEC controller that sets and stabilizes a TEC temperature. A voltage applied to the input of the SLM8834 corresponds to the temperature setpoint of the target object attached to the TEC. The SLM8834 controls an internal FET H-bridge whereby the direction of the current fed through the TEC can be either positive (for cooling mode), to pump heat away from the object attached to the TEC, or negative (for heating mode), to pump heat into the object attached to the TEC. Temperature is measured with a thermal sensor attached to the target object and the sensed temperature (voltage) is fed back to the SLM8834 to complete a closed thermal control loop of the TEC. For the best overall stability, couple the thermal sensor close to the TEC. In most laser diode modules, a TEC and a NTC thermistor are already mounted in the same package to regulate the laser diode temperature.

The TEC is differentially driven in an H-bridge configuration. The SLM8834 drives its internal MOSFET transistors to provide the TEC current. To provide good power efficiency and zero crossing quality, only one side of the H-bridge uses a PWM driver. Only one inductor and one capacitor are required to filter out the switching frequency. The other side of the H-bridge uses a linear output without requiring any additional circuitry. This proprietary configuration allows the SLM8834 to provide efficiency of >90%. For most applications, a 1 μH inductor, a 10 μF capacitor, and a switching frequency of 2 MHz maintain less than 1% of the worst-case output voltage ripple across a TEC.

The maximum voltage across the TEC and the current flowing through the TEC are set by using the VLIM/SD and ILIM pins. The maximum cooling and heating currents can be set independently to allow asymmetric heating and cooling limits. For additional details, see the [Maximum TEC Voltage Limit](#page-14-3) section and the [Maximum TEC Current Limit](#page-14-5) section.

### <span id="page-12-1"></span>**ANALOG PID CONTROL**

The SLM8834 integrates two self-correcting, autozeroing amplifiers (Chopper 1 and Chopper 2). The Chopper 1 amplifier takes a thermal sensor input and converts or regulates the input to a linear voltage output. The OUT1 voltage is proportional to the object temperature. The OUT1 voltage is fed into the compensation amplifier (Chopper 2) and is compared with a temperature setpoint voltage, which creates an error voltage that is proportional to the difference. For autonomous analog temperature control, Chopper 2 can be used to implement a PID network as shown in [Figure 2](#page-1-1) to set the overall stability and response of the thermal loop. Adjusting the PID network optimizes the step response of the

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TEC control loop. A compromised settling time and the maximum current ringing become available when this adjustment is done.

### <span id="page-12-2"></span>**DIGITAL PID CONTROL**

The SLM8834 can also be configured for use in a software controlled PID loop. In this scenario, the Chopper 1 amplifier can either be left unused or configured as a thermistor input amplifier connected to an external temperature measurement analog-todigital converter (ADC). If Chopper 1 is left unused, tie IN1N and IN1P to AGND. The Chopper 2 amplifier is used as a buffer for the external DAC, which controls the temperature setpoint. Connect the DAC to IN2P and short the IN2N and OUT2 pins together. See [Figure 3](#page-1-2) for an overview of how to configure the SLM8834 external circuitry for digital PID control.

### <span id="page-12-3"></span>**POWERING THE CONTROLLER**

The SLM8834 operates at an input voltage range of 2.7 V to 5.5 V that is applied to the VDD pin and the PVIN pin for the WLCSP (the PVINS pin and PVINL pin for the LFCSP). The VDD pin is the input power for the driver and internal reference. The PVIN input power pins are combined for both the linear and the switching driver. Apply the same input voltage to all power input pins: VDD and PVIN. In some circumstances, an RC lowpass filter can be added optionally between the PVIN for the WLCSP (PVINS and PVINL for the LFCSP) and VDD pins to prevent high frequency noise from entering VDD, as shown in [Figure 3.](#page-1-2) The capacitor and resistor values are typically 10 Ω and 100 nF, respectively. When configuring power supply to the SLM8834, keep in mind that at high current loads, the input voltage may drop substantially due to a voltage drop on the wires between the front-end power supply and the PVIN for the WLCSP (PVINS and PVINL for the LFCSP) pin. Leave a proper voltage margin when designing the front-end power supply to maintain the performance. Minimize the trace length from the power supply to the PVIN for the WLCSP (PVINS and PVINL for the LFCSP) pin to help mitigate the voltage drop.

### <span id="page-12-4"></span>**ENABLE AND SHUTDOWN**

To enable the SLM8834, apply a logic high voltage to the EN/SY pin while the voltage at the VLIM/SD pin is above the maximum shutdown threshold of 0.07 V. If either the EN/SY pin voltage is set to logic low or the VLIM/SD voltage is below 0.07 V, the controller goes into an ultralow current state. The current drawn in shutdown mode is 350 μA typically. Most of the current is consumed by the VREF circuit block, which is always on even when the device is disabled or shut down. The device can also be enabled when an external synchronization clock

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signal is applied to the EN/SY pin, and the voltage at VLIM/SD input is above 0.07 V. [Table 1](#page-13-5) shows the combinations of the two input signals that are required to enable the SLM8834.

<span id="page-13-5"></span>Table 1. Enable Pin Combinations



<sup>1</sup> No effect means this signal has no effect in shutting down or in enabling the device.

## <span id="page-13-0"></span>**OSCILLATOR CLOCK FREQUENCY**

The SLM8834 has an internal oscillator that generates a 2.0 MHz switching frequency for the PWM output stage. This oscillator is active when the enabled voltage at the EN/SY pin is set to a logic level higher than 2.1 V and the VLIM/SD pin voltage is greater than the shutdown threshold of 0.07 V.

## <span id="page-13-1"></span>**EXTERNAL CLOCK OPERATION**

The PWM switching frequency of the SLM8834 can be synchronized to an external clock from 1.85 MHz to 3.25 MHz, applied to the EN/SY input pin as shown on [Figure 13.](#page-13-6)



<span id="page-13-6"></span>Figure 13. Synchronize to an External Clock

## <span id="page-13-2"></span>**CONNECTING MULTIPLE SLM8834 DEVICES**

Multiple SLM8834 devices can be driven from a single master clock signal by connecting the external clock source to the EN/SY pin of each slave device. The input ripple can be greatly reduced by operating the SLM8834 devices 180° out of phase from each other by placing an inverter at one of the EN/SY pins, as shown in [Figure 14.](#page-13-7)





<span id="page-13-7"></span>

### <span id="page-13-3"></span>**TEMPERATURE LOCK INDICATOR (LFCSP ONLY)**

The TMPGD outputs logic high when the temperature error amplifier output voltage, Vout1, reaches the IN2P temperature setpoint (TEMPSET) voltage. The TMPGD has a detection range between 1.46 V and 1.54 V of  $V_{\text{OUT1}}$  and hysteresis. The TMPGD function allows direct interfacing either to the microcontrollers or to the supervisory circuitry.

### <span id="page-13-4"></span>**SOFT START ON POWER-UP**

The SLM8834 has an internal soft start circuit that generates a ramp with a typical 80 ms profile to minimize inrush current during power-up. The settling time and the final voltage across the TEC depends on the TEC voltage required by the control voltage of voltage loop. The higher the TEC voltage is, the longer it requires to be built up.

When the SLM8834 is first powered up, the linear side discharges the output of any prebias voltage. As soon as the prebias is eliminated, the soft start cycle begins. During the soft start cycle, both the PWM and linear outputs track the internal soft start ramp until they reach midscale, where the control voltage,  $V_c$ , is equal to the bias voltage,  $V_B$ . From the midscale voltage, the PWM and linear outputs are then controlled by  $V_c$  and diverge from each other until the required differential voltage is developed across the TEC or the differential voltage

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reaches the voltage limit. The voltage developed across the TEC depends on the control point at that moment in time. [Figure 15](#page-14-7) shows an example of the soft start in cooling mode. Note that, as both the LDR and SFB voltages increase with the soft start ramp and approach  $V_B$ , the ramp slows down to avoid possible current overshoot at the point where the TEC voltage starts to build up.



Figure 15. Soft Start Profile in Cooling Mode

### <span id="page-14-7"></span><span id="page-14-0"></span>**TEC VOLTAGE/CURRENT MONITOR**

The TEC real-time voltage and current are detectable at VTEC and ITEC, respectively.

### <span id="page-14-1"></span>**VOLTAGE MONITOR**

VTEC is an analog voltage output pin with a voltage proportional to the actual voltage across the TEC. A center VTEC voltage of 1.25 V corresponds to 0 V across the TEC. Convert the voltage at VTEC and the voltage across the TEC using the following equation:

*VVTEC = 1.25 V + 0.25 × (VLDR − VSFB)*

#### <span id="page-14-2"></span>**CURRENT MONITOR**

ITEC is an analog voltage output pin with a voltage proportional to the actual current through the TEC. A center ITEC voltage of 1.25 V corresponds to 0 A through the TEC. Convert the voltage at ITEC and the current through the TEC using the following equations:

 $V_{\text{ITEC}}$  cooling = 1.25 V +  $I_{\text{LDR}} \times R_{\text{CS}}$ where the current sense gain ( $Rcs$ ) is 0.525 V/A. *VITEC\_HEATING = 1.25 V − ILDR × RCS*

#### <span id="page-14-3"></span>**MAXIMUM TEC VOLTAGE LIMIT**

The maximum TEC voltage is set by applying a voltage divider at the VLIM/SD pin to protect the TEC. The voltage limiter operates bidirectionally and allows the cooling limit to be different from the heating limit.

#### <span id="page-14-4"></span>**USING A RESISTOR DIVIDER TO SET THE TEC VOLTAGE LIMIT**

Separate voltage limits are set using a resistor divider. The internal current sink circuitry connected to VLIM/SD draws a current when the SLM8834

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drives the TEC in a heating direction, which lowers the voltage at VLIM/SD. The current sink is not active when the TEC is driven in a cooling direction; therefore, the TEC heating voltage limit is always lower than the cooling voltage limit.





Calculate the cooling and heating limits using the following equations:

 $V_{VLIM\_COOLING} = V_{REF} \times R_{V2}/(R_{V1} + R_{V2})$ where  $V_{REF} = 2.5 V$ .

*VVLIM\_HEATING = VVLIM\_COOLING* <sup>−</sup> *ISINK\_VLIM × RV1||RV2* where  $I_{SINK_VLIM}$  = 10 μA. *VTEC\_MAX\_COOLING = VVLIM\_COOLING × AVLIM* where  $A_{VLIM} = 2 V/V$ . *VTEC\_MAX\_HEATING = VVLIM\_HEATING × AVLIM*

### <span id="page-14-5"></span>**MAXIMUM TEC CURRENT LIMIT**

To protect the TEC, separate maximum TEC current limits in cooling and heating directions are set by applying a voltage combination at the ILIM pin.

#### <span id="page-14-6"></span>**USING A RESISTOR DIVIDER TO SET THE TEC CURRENT LIMIT**

The internal current sink circuitry connected to ILIM draws a 40 μA current when the SLM8834 drives the TEC in a cooling direction, which allows a high cooling current. Use the following equations to calculate the maximum TEC currents:

*VILIM\_HEATING = VREF × RC2/(RC1 +RC2)* where  $V_{REF} = 2.5 V$ . *VILIM\_COOLING = VILIM\_HEATING + ISINK\_ILIM × RC1||RC2* where  $I_{SINK ILIM} = 40 \mu A$ .

$$
I_{TEC\_MAX\_COOLING} = \frac{V_{ILIM\_COOLING} - 1.25 \text{ V}}{R_{CS}}
$$

where  $R_{CS} = 0.525$  V/A.



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 $1.25~{\rm V}-V_{lllM\_{HEATING}}$  $I_{\textit{\tiny TEC}\_\textit{MAX}\_\textit{\tiny HEATING}}\,=\,$  $R_{CS}$ 

VILIM\_HEATING MUSt not exceed 1.2 V and VILIM\_COOLING must be more than 1.3 V to leave proper margins between the heating and the cooling modes.



Figure 17. Using a Resistor Divider to Set the TEC Current Limit

## <span id="page-16-0"></span>**CLASSIFICATION REFLOW PROFILS**





Figure 18. Classification Profile



## <span id="page-17-0"></span>**PACKAGE INFORMATION**



Figure 19. 25 ball, 2.5mm x 2.5mm WLCSP Outline Dimensions



Figure 20. 24 Lead, 4mm x 4mm QFN Outline Dimensions

## <span id="page-18-0"></span>**REVISION HISTORY**

Note: page numbers for previous revisions may differ from page numbers in current version

